ADVANCED SURFACE-REFLECTED RADIANCE CORRECTION FOR AIRBORNE HYPERSONTAL IMAGERY IN COASTAL RED TIDE DETECTION

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ABSTRACT:

Red tides are among the most common coastal hazards, causing serious damage to the coastal environment. Many satellite sensors can detect red tide blooms, but are limited in their detection of the exact area of the bloom and biological abundance in terms of spatial and spectral resolution. The high spatial and spectral resolutions of hyperspectral airborne remote sensing data may help overcome these limitations to analyze red tide blooms more effectively. To identify potential applications of hyperspectral airborne data in red tide detection, an integrated field campaign was performed in September 2016 off the coast of Tongyeong, South Korea. An AisaEAGLE sensor was installed on a Cessna 208B crewed aircraft to obtain hyperspectral images of an 18 km × 18 km coastal area. To assess the atmospheric correction of the hyperspectral data, in situ optical data and water samples were measured on two vessels concurrent with the flight path. Advanced surface-reflected radiance (L_r) correction and basic atmospheric path radiance (L_a) correction were performed on the hyperspectral images. Of these, L_r correction comprised a large proportion of the atmospheric correction. The atmosphere-corrected remote sensing reflectance data of the hyperspectral images closely matched the in-situ measurements. The data were assessed for red tide events using ratio analysis and the fluorescence line height technique; the ratio analysis more effectively detected regions with suspected red tides.

1. INTRODUCTION

Red tides, a common name for harmful algal bloom, are among the most common coastal disasters, causing serious damage to the coastal marine environment in South Korea (Kim et al., 2004; Lee et al., 2013). Although many satellite sensors are capable of detecting red tides, they are limited in their abilities to accurately analyze the exact shape and area of the red tide patch and the biological abundance in terms of spatial and spectral resolution. Aircraft-mounted hyperspectral sensors may overcome these limitations because of their high spatial and spectral resolutions, while remaining more cost-effective.

Imaging spectrometry (i.e., hyperspectral imaging) began at the Jet Propulsion Laboratory of the National Aeronautics and Space Administration (NASA) in the early 1980s, and enabled the acquisition of images on continuous spectrum channels. This method provides complete reflectivity spectrum information within a wavelength region for each pixel within an area (Gao et al., 2009). Hyperspectral remote sensing, which provides information regarding the overall spectral spectrum of the object, has been used for terrestrial studies in various fields (e.g., geology, mineralogy, agriculture, and forestry). In recent decades, it has also been applied to coastal and inland water quality research (Thiemann and Kaufmann, 2002; Brando and Dekker, 2003; Karaska et al., 2004; Vahtmae et al., 2006; Giardino et al., 2007; Ryan et al., 2009; Olmanson et al., 2013; Guild et al., 2020; Shin et al., 2020). However, it is difficult to use airborne hyperspectral imaging data for coastal environment analysis. Due to the comparatively large field of view (FOV) and complex pixel-based geometry, various pre-processing steps are required, and data verification is important. Due to these difficulties, a simple atmospheric correction based on radiative transfer model or provided on SW was used for the coastal ecosystem monitoring using aerial remote sensing data (Guild et al., 2020; Shin et al., 2020). In addition, for some data obtained at low altitudes, atmospheric correction was not performed (Guild et al., 2020). In this study, compared with the atmospheric correction using existing radiative transfer models, the advanced atmospheric correction was applied by correcting the angular reflected radiation on the sea surface to enable effective detection of red tide blooms using hyperspectral datasets.

2. METHODOLOGY

2.1 Study area and data acquisition

The study was performed in Tongyeong, South Korea, which is known for its high occurrence of red tides in summer. It also hosts the largest fish farms in South Korea, and experiences the greatest damage from red tide blooms (Lee et al., 2013). The field campaign for the acquisition and verification of hyperspectral
images was conducted on September 24, 2016, in the coastal area
of Tongyeong. Figure 1 shows the location of the study area and
the planned aircraft flight path. Hyperspectral images were
acquired with an AisaEAGLE hyperspectral sensor (Specim,
Spectral Imaging Ltd., Oulu, Finland) mounted on a crewed
Cessna 208B (Cessna, Wichita, KS, USA) operated by ASIA
Aero Survey Co., Ltd. (Seoul, South Korea) (Figure 2). Table 1
lists detailed information regarding the aircraft and sensor.
Because AisaEAGLE is a push-broom scanning linear sensor, 10
line-scan images with 30% sidelap were obtained in the 18 km ×
18 km study area (Figure 3). The spatial resolution was 2.0 m,
because of the flight height of 3,000 m, and approximately 130
bands of spectral data were measured within 400–1000 nm.

To verify the obtained hyperspectral images, match-up
data were measured on two vessels at the same time and location as
the corresponding flight route scheduled from 09:00 to 12:00 on
September 24, 2016. In total, eight match-up datasets were
obtained for the hyperspectral data verification. Water and sky
radiance on the sea surface were measured using a
spectroradiometer (ASD FieldSpec-3; Malvern Panalytical,
Malvern, UK) to verify the result of atmospheric correction
(Figure 4a). The marine environmental information included the
absorption coefficients of sea water components for chlorophyll,
suspended particulate matter (SPM), and dissolved organic
matter (DOM), as well as the concentrations of chlorophyll (Cph)
and SPM (CSPM) (Figure 4b). A spectrophotometer (Cary 100;
Agilent, Santa Clara, CA, USA) was used to measure the
absorption coefficients of total particles (aTota), SPM (aSPM),
and DOM (aDOM). The absorption coefficient of chlorophyll (aph)
was calculated by subtracting aSPM from aTota. Cph was calculated
using the trichroic equation (Jeffrey and Humphrey, 1975) and
CSPM was measured gravimetrically after filtration on pre-dried
(60°C, 4 h) 47-mm polycarbonate membrane filters. All data
acquisition methods and calculations were performed in
accordance with the NASA Ocean Optics Protocols (Mueller et
al., 2003) and International Ocean Colour Coordinating Group
(IOCCG) Protocol Series (Boss et al., 2018).

Table 1. Information regarding the Cessna 208B aircraft and
AisaEAGLE hyperspectral sensor.

<table>
<thead>
<tr>
<th>Aircraft</th>
<th>Cessna 208B</th>
</tr>
</thead>
<tbody>
<tr>
<td>Size (W × L × H)</td>
<td>15.9 m ×12.7 m × 4.7 m</td>
</tr>
<tr>
<td>Weight (empty)</td>
<td>2,067 kg</td>
</tr>
<tr>
<td>Maximum weight</td>
<td>3,969 kg</td>
</tr>
<tr>
<td>Operation Speed</td>
<td>Minimum 120 kn (222 km/h)</td>
</tr>
<tr>
<td>Maximum 185 kn (343 km/h)</td>
<td></td>
</tr>
<tr>
<td>Flying Range</td>
<td>Maximum 1,996 km</td>
</tr>
<tr>
<td>Flying Height</td>
<td>Maximum 7,620 m</td>
</tr>
</tbody>
</table>

<table>
<thead>
<tr>
<th>Sensor</th>
<th>AisaEAGLE</th>
</tr>
</thead>
<tbody>
<tr>
<td>Spectral range</td>
<td>400 – 1,000 nm</td>
</tr>
<tr>
<td>Spectral band</td>
<td>Maximum 488 bands</td>
</tr>
<tr>
<td>Spatial pixels</td>
<td>1,024 pixels</td>
</tr>
<tr>
<td>Swath width</td>
<td>2,048 m (at a height of 3,000 m)</td>
</tr>
<tr>
<td>Ground Resolution</td>
<td>2 m (at a height of 3,000 m)</td>
</tr>
<tr>
<td>Data interface</td>
<td>12 bits Cameralink</td>
</tr>
</tbody>
</table>
Atmospheric correction was performed in two steps. Generally, an aircraft-mounted sensor viewing the ocean measures upwelling radiance that includes contributions by the atmosphere, water surface, and water column (Mobley et al., 2020), as illustrated in Figure 6. Atmospheric path radiance \( L_a \) is the atmospheric scattering effect caused by solar radiance scattered one or more times by atmospheric gases and aerosols into the direction of the sensor. Sun- or sky-radiance (i.e., sun and sky glint; \( L_s \)) represents downwelling solar radiance reflected toward the sensor off the water surface. When the light source is transmitted through the surface in the ocean (\( L_w \)), it is altered by absorbing and scattering components in the water. \( L_a \) is then scattered upward and transmitted back through surface toward the sensor as water-leaving radiance \( L_{w+} \). Total radiance \( L_u \) represents the sensor scanning data, including the atmospheric contributions of \( L_a \) and \( L_s \), as well as \( L_w \) (the value of interest in this study). To obtain \( L_{w+} \), \( L_a \) and \( L_s \) were subtracted from \( L_u \) (Eq. 1). In this study, \( L_s \) was corrected using the Atmospheric and Topographic CORrection (ATCOR) software (ReSe Applications, Wil, Switzerland), based on MODTRAN5 modeling. \( L_w \) was corrected using in situ sky radiance \( L_{w+} \) and the surface reflection model proposed by Mobley et al. (2015).

2.2 Hyperspectral data pre-processing

The raw data (digital number) captured by the hyperspectral camera were processed sequentially for radiometric correction, georeferencing, atmospheric correction, and mosaic processing. Figure 5 presents the data processing procedure. First, radiometric and geometric corrections were performed using CaligeoPRO software (Specim, Spectral Imaging Ltd.). Radiometric correction was initially accomplished to compensate for the scattering of radiation due to atmospheric scattering, the geometrical relationship between target and sensor, and the sensor response characteristics. Then, geometric correction was performed using the Global Positioning System/Inertial Navigation System (GPS/INS) and calibration dataset. In this process, the coordinate information of each pixel was obtained by synchronizing the image with the GPS/INS data to generate an orthorectified image.

### Table 2: Information regarding hyperspectral image acquisition.

<table>
<thead>
<tr>
<th>Scan Line #</th>
<th>Scan time local hh:mm</th>
<th>Scan order</th>
<th>Zenith (-18.85° - 18.89°)</th>
<th>Flight direction</th>
<th>Azimuth (°)</th>
<th>Solar geometry (°)</th>
<th>( \psi (°) )</th>
<th>Surface reflectance factors ( \rho ) by Mobley's model (Figure 8)</th>
</tr>
</thead>
</table>
|             |                        |            |                           |                 | Upper       | Lower             | Azimuth Elevation | Upper       | Lower         | \( \r
| 1           | 10:40                  | 1          | +                         | -               | to West     | 4.2               | 184.2               | 141.58      | 47.82          | 222.62        | 42.62          | 0.12          | 0.12          | 0.09          | 0.06          | 0.04          |
| 2           | 10:55                  | 3          | +                         | -               | to West     | 301.6             | 121.6               | 146.56      | 49.62          | 155.04        | -24.96         | 0.14          | 0.14          | 0.09          | 0.06          | 0.04          |
| 3           | 11:10                  | 5          | +                         | -               | to West     | 1.8               | 181.8               | 151.91      | 51.20          | 209.89        | 29.89          | 0.14          | 0.14          | 0.09          | 0.06          | 0.04          |
| 4           | 10:48                  | 2          | -                         | +               | to East     | 357.7             | 177.7               | 144.19      | 48.81          | 213.51        | 33.51          | 0.14          | 0.14          | 0.09          | 0.06          | 0.04          |
| 5           | 11:03                  | 4          | -                         | +               | to East     | 357.9             | 177.9               | 149.37      | 50.49          | 208.53        | 28.53          | 0.14          | 0.14          | 0.09          | 0.06          | 0.04          |
| 6           | 12:27                  | 10         | +                         | -               | to West     | 1.9               | 181.9               | 183.60      | 54.60          | 178.3         | -1.7           | 0.2           | 0.2           | 0.09          | 0.05          | 0.04          |
| 7           | 11:32                  | 7          | -                         | +               | to East     | 358.2             | 178.2               | 160.36      | 53.02          | 197.84        | 17.84          | 0.2           | 0.2           | 0.09          | 0.05          | 0.04          |
| 8           | 11:47                  | 9          | -                         | +               | to East     | 358.1             | 178.1               | 166.49      | 53.90          | 191.61        | 11.61          | 0.2           | 0.2           | 0.09          | 0.05          | 0.04          |
| 9           | 11:26                  | 6          | +                         | -               | to West     | 1.8               | 181.8               | 157.99      | 52.58          | 203.81        | 23.81          | 0.14          | 0.14          | 0.09          | 0.06          | 0.04          |
| 10          | 11:40                  | 8          | +                         | -               | to West     | 1.8               | 181.8               | 163.60      | 53.53          | 198.2         | 18.2           | 0.2           | 0.2           | 0.09          | 0.05          | 0.04          |
ATCOR software provides atmospheric and topographic corrections to eliminate atmospheric and topographic effects and derive physical values from the Earth’s surface, such as surface reflectivity spectra, radiation rates, and surface temperatures (Richter and Schläpfer, 2017). There are three ATCOR models available, two for satellite imagery (ATCOR-2 and -3) and one for airborne imagery (ATCOR-4), where the numbers 2–4 represent the geometric degrees of freedom (DOF). ATCOR-2 and -3 were developed for satellite imagery of flat terrain (2 geometric DOF) and mountainous terrain (3 geometric DOF), respectively. By contrast, ATCOR-4 includes 4 geometric DOF for x, y, z, and scan angle, among which scan angle is important for correcting atmospheric effects of airborne images because most airborne sensors have a large FOV.

Input image and scan angle files are required for ATCOR processing. The scan angle file was generated with CaligeoPRO software (Figure 5) using the “ATCOR4f: flat terrain” mode to represent marine data. Next, the sensor type, flight operation information, and solar geometry values were set for sensor and calibration file generation (detailed information is listed in Table 2), and the ‘maritime’ aerosol type was selected. Finally, $L_{\omega}$-corrected data from total radiance were obtained.

2.3 Correction of Surface-reflected radiance ($L_{\omega}$)

$L_{\omega}$ is a function of viewing direction ($\theta$), azimuth angle ($\varphi$), and wavelength ($\lambda$); it encompasses $L_{\omega}$ and $L_{\omega}$ as well as $L_{\omega}$ (the parameter of interest in this study), as shown in Eq. (1). $L_{\omega}$ was easily removed using ATCOR. However, $L_{\omega}$ consists of three components (Figure 7): direct solar reflection (i.e., sun glint; $L_{\omega}$, Figure 7), sun and sky reflection values from adjacent pixels ($L_{\omega}$, Figure 7), and sky-reflected radiance ($L_{\omega}$, Figure 7).

Sun glint is a mirror-like specular reflection of sunlight reflected off water back at the sensor, which occurs when sunlight reflects off the surface of water at an angle identical to the angle at which the satellite sensor views it. Sun glint ($L_{\omega}$) was eliminated because it comprises a large proportion of $L_{\omega}$. The white area at the bottom of each scan line represents the sun-glint region (Figure 3). Large sun-glint regions were observed in the images obtained in this study, which expanded as time approached noon and the sun’s elevation increased. In this study, calibration was achieved by eliminating values $\geq 0.0035$ in the NIR band of 865 nm. Sun and sky reflection from adjacent pixels ($L_{\omega}$) is difficult to calibrate, and was thus not calibrated in this study. Finally, sky-reflected radiance ($L_{\omega}$) was corrected using in situ $L_{\omega}$ data and a surface reflection model. $L_{\omega}$ can be modelled as the product of surface radiance reflection ($\rho$) multiplied by $L_{\omega}$, as shown in Eq. (2).

$$L_{\omega}(\theta, \varphi, \lambda) = L_{\omega}(\theta, \varphi, \lambda) - L_{\omega}(\theta, \varphi, \lambda) - L_{\omega}(\theta, \varphi, \lambda) \quad (1)$$

$$L_{\omega}(\theta, \varphi, \lambda) = L_{\omega}(\theta, \varphi, \lambda) - L_{\omega}(\theta, \varphi, \lambda) - \rho(\theta, \varphi, \theta_{0}, W) L_{\omega}(\theta, \varphi, \lambda) \quad (2)$$

where $\theta$: viewing direction (zenith angle) for each pixel
(same as $\theta_{0}$ in Mobley’s model)
$\varphi$: azimuth angle for each pixel from the North direction
$\theta_{0}$: solar zenith angle
$\rho$: radiance reflection
$\lambda$: wavelength

Figure 7. Conceptual diagram of the surface-reflected radiance ($L_{\omega}$).

Figure 8. Surface radiance reflection ($\rho$) as a function of off-nadir and azimuthal viewing directions (relative to the sun’s azimuth at $\varphi_{0} = 0$) for a single sun zenith angle of $\theta_{0} = 40^\circ$, computed using FFT surface and polarized ray tracing with a Rayleigh sky and a wind speed of 10 m s$^{-1}$ (Mobley, 2015).

Mobley (2015) generated $\rho$ at the sea surface as a function of viewing direction and azimuth angle of the sensor, solar zenith angle, and wind speed. Figure 8 shows the $\rho$ modelling result as a function of sensor viewing angle from nadir and sensor azimuth angle from the sun in the case of a fixed solar zenith angle ($\theta_{0}$) of 40° and wind speed of 10 m s$^{-1}$. Because the sensor viewing angles for pixels were distributed between $\sim 18.85^\circ$ and $18.89^\circ$, $\rho$ values within the red dotted line in Figure 8 were used for $L_{\omega}$ correction. According to the relative azimuth angle from the sun to the sensor ($\varphi_{0}$) for each scan line, the $\rho$ values were extracted from Figure 8 and listed in Table 2. $L_{\omega}$ was calculated using the extracted $\rho$ values (Table 2) and in situ $L_{\omega}$ data. Both $L_{\omega}$ and $L_{\omega}$ were subtracted from $L_{\omega}$ to obtain $L_{\omega}$. Finally, remote sensing reflectance ($R_{\omega}$) was calculated by dividing $L_{\omega}$ into in situ downwelling radiance.

This contribution has been peer-reviewed. The double-blind peer-review was conducted on the basis of the full paper.

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3. RESULTS

3.1 Verification of atmospheric correction results

Figure 9 shows the mosaic $R_s$ image of atmosphere-corrected hyperspectral scanning data for path radiance and surface reflection. Compared with the uncorrected images (Figure 3), the sun-glint region and high-reflection regions were well corrected. The atmosphere-corrected results were verified using in situ $R_s$ data, which matched the airborne images. In total, eight sets of in situ data were acquired, but two datasets were not matched with the airborne data because of cloud masking. The sampling locations of the match-up data are illustrated by red crosses in Figure 9, and the obtained in situ $R_s$ spectrum is displayed as a green line in Figure 10. Stations st01 and st07 were located at the upper part of the line, which was comparatively strongly affected by sun glint, whereas stations st02, st04, st06, and st08 were located at the lower part of the line, which was comparatively unaffected by sun glint. The in-situ $R_s$ spectrum was compared with $L_r$-corrected (blue line, Figure 10) and $L_r+L_s$-corrected (red line, Figure 10) results. The $L_r$-corrected $R_s$ spectrum showed values $2 \sim 3$-fold higher than the in-situ dataset throughout the wavelength range. By contrast, the $L_r+L_s$-corrected $R_s$ spectrum had values similar to the in-situ $R_s$ data, and effectively eliminated atmospheric effects.

The shapes of the $L_r$-corrected and $L_r+L_s$-corrected $R_s$ spectra were similar to the shape of the in situ $R_s$ spectrum throughout the wavelength range. Notably, $L_r$-corrected $R_s$ at st08 was almost identical to the in situ $R_s$ data. However, there were small differences within the wavelength range of 450 $\sim$ 550 nm, especially at stations located at the upper part of the line (st01 and st07, Figure 10a and c). For stations located at the lower part of the line (st02, st04, st06, and st08, Figure 10b, c, d, and f), the $R_s$ values were eliminated more within 450 $\sim$ 500 nm than at other wavelengths. With respect to st04, located within the area most affected by sun glint, the atmospheric effect was over-corrected within 450 $\sim$ 500 nm, with $R_s$ values smaller than values in the in-situ $R_s$ data. This result was due to excessive correction of $L_r$. By contrast, within 650 $\sim$ 750 nm, less $L_r$ correction was applied than at other wavelengths. Overall,
The Rs spectrum verification confirmed the effectiveness of the atmospheric correction, especially at wavelengths of 550 ~ 650 nm, as well as the similar shapes and values of the corrected Rs spectra compared with the in-situ Rs spectrum.

### 3.2 Red tide detection

We had planned to conduct the airborne hyperspectral imaging campaign during a red tide bloom. However, the bloom ended before the campaign, and therefore data collection was carried out in the absence of a bloom. Regardless, areas of potential red tide blooms were observed in the atmosphere-corrected hyperspectral imagery. In Figure 9, the areas marked with two red boxes and one yellow box represent regions with potential red tides (hereafter, red tide-suspected regions). To analyze and compare the Rs spectra for red tide blooms with the spectra of other turbid water or clear water, the Rs spectra were extracted from areas within the three red tide-suspected regions, three turbulent water regions, and three clear water regions. The extracted Rs spectra are presented in Figure 11a, and Figure 11b shows the patches used for Rs spectrum extraction. The relative position of each patch is shown in Figure 9 as a box of the same color. The Rs values fell within a defined range without particular abnormal values, and the Rs spectral shapes differed for each type of region. Large Rs values within the wavelength range of ≥ 750 nm were excluded from the red tide analysis due to the poor performance of atmospheric correction at these wavelengths.

The Rs spectra of red tide-suspected regions and regions with no red tides (i.e., turbid and clear water) were separated, and are displayed in Figure 12. Two notable differences were observed. First, the Rs spectra for the red tide-suspected regions showed an increasing slope within the wavelength range of 547 ~ 575 nm, whereas the non-red tide regions showed a decreasing slope. Second, comparatively large and prominent peaks were observed at 680 nm, which is affected by chlorophyll fluorescence, in the Rs spectra from red tide-suspected regions.

![Figure 12. Comparison of the Rs spectra from (a) red tide-suspected regions and (b) other regions (i.e., other turbid water and clear water).](image)

![Figure 13. Red tide detection based on (a, b) fluorescence line height analysis at 680 nm and (c, d) ratio analysis between 547 and 575 nm.](image)
To assess the potential for red tide detection using hyperspectral images, ratio analysis using $R_n$ values of 547 and 575 nm and fluorescence line height (FLH) analysis at 680 nm were performed. The ratio analysis was calculated by dividing the $R_n$ value at 547 nm by the $R_n$ value at 575 nm. Figures 13c and d show the ratio analysis results; red shading in Figure 13d with values greater than 1 indicates red tide-suspected regions. The FLH analysis was calculated using two base wavelengths at 657 and 731 nm, along with one peak wavelength at 683 nm. Figures 13a and b show the FLH analysis results; red shading in Figure 13b indicates red tide-suspected regions. Of these two methods, the ratio analysis more effectively estimated the red tide-suspected regions, whereas the FLH analysis mis-detected some coastal turbid areas (yellow circle, Figure 13b and d).

4. CONCLUSIONS

In this study, an integrated field campaign was performed for the acquisition of airborne hyperspectral images combined with in situ match-up data measurements for red tide detection. For the atmospheric correction of hyperspectral images, $L_a$ and surface reflection of $L_{rs}$ (i.e., $L_s$) were eliminated from the total radiance. Additionally, land, cloud, and sun-glint areas were removed from the images. $L_a$ correction based on the aircraft characteristics and the relative geometry of each pixel using ATCOR was remarkably successful, when combined with $L_s$ correction using the surface reflection model developed by Mobley (2015). In particular, $L_a$ correction comprised a large proportion of the atmospheric correction because airborne measurements have a wide FOV. Red tide detection was analyzed using two methods, ratio analysis of the FLH technique, of which the ratio analysis more effectively predicted red tide-suspected regions.

Airborne hyperspectral imaging has many advantages in coastal red tide analysis, including the observation of large areas of coastal waters with high spatial resolution and the freedom of measuring areas of interest. In addition, spectral bands not provided by ocean color sensors could be used based on the spectral characteristics of red tides, enabling effective detection of red tide blooms. However, hyperspectral images contain large amounts of data, requiring high-end hardware and substantial time for data processing. Furthermore, precise atmospheric correction is required, considering the relative geometric position of each pixel. In this study, we found that airborne observations were heavily influenced by surface reflected radiance due to the wide FOV. At the flight planning stage, orienting the flight in the east–west direction greatly influenced surface reflection and made correction difficult. Future airborne observations should design flight plans considering the position of the sun. Moreover, based on Mobley’s model, it would be appropriate to set a solar–sensor azimuth between 60° and 120°.

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REFERENCES


